MUTHAYAMMAL ENGINEERING COLLEGE
(An Autonomous Institution)
(Approved by AICTE, New Delhi, Accredited by NAAC \& Affiliated to Anna University)
Rasipuram - 637 408, Namakkal Dist., Tamil Nadu.

MUST KNOW CONCEPTS
CIVIL
2020-21

Course code \& Course Name : 19CED02 \& Mechanics of Solids
Year/Sem/Sec : II/III

| S.NO | Term | Notation (Symbol) | Concept/Definition/Meaning/Units/Equati on/Expression | Units |
| :---: | :---: | :---: | :---: | :---: |
| UNIT I STRESS AND STRAIN |  |  |  |  |
| 1 | Strain | e | Change in length by original length when load is applied (dL/L) dL = pL/Ae | No Unit |
| 2 | Young's Modulus | E | Stress/Strain | $\mathrm{N} / \mathrm{mm}^{2}$ |
| 3 | Bulk modules | K | Stress /Volumetric strain $K=\sigma / \mathrm{e}_{\mathrm{v}}$ | $\mathrm{N} / \mathrm{mm}^{2}$ |
| 4 | Poisson's ratio | $\mu$ | Lateral or secondary strain / linear or primary strain $=1 / \mathrm{m}$ | No unit |
| 5 | Volumetric strain | $\mathrm{e}_{\mathrm{v}}$ | Change in volume / original volume dv/v | No unit |
| 6 | Relationshi pb/w young's and Bulk modulus |  | $E=3 K(1-2 / m)$ | $\mathrm{N} / \mathrm{mm}^{2}$ |
| 7 | Modulus of rigidity | G, N or G | Ratio of shear stress to shear strain $\tau / \mathrm{e}_{\text {s }}$ | $\mathrm{N} / \mathrm{mm}^{2}$ |
| 8 | Longitudin al strain | e | Stress/ young's modulus $\mathrm{e}=\mathrm{\sigma} / \mathrm{E}$ | No unit |
| 9 | Compressiv e stress | $\sigma$ | Compressive load / Area= P/A | $\mathrm{N} / \mathrm{mm}^{2}$ |
| 10 | Thermal strain | e | A actual expansion allowed/ original length (aTL-s) /L | No unit |
| 11 | Thermal stress | $\sigma$ | Thermal strain X Young's modulus $\sigma$ $=((\alpha T L-s) / L) X E$ | $\mathrm{N} / \mathrm{mm}^{2}$ |
| 12 | Tensile strain | $\mathrm{e}_{1}$ | The Increment of length to its actual length $\mathrm{e}_{\mathrm{l}}=\partial \mathrm{L} / \mathrm{L}$ | No unit |
| 13 | Lateral strain | $e_{t}$ | Change in breadth (depth)/Original breadth (depth) ( $\partial \mathbf{b} / \mathrm{b}$ or $\partial \mathbf{d} / \mathrm{d}$ ) | No unit |


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| 14 | Strain energy | U | The strain energy stored by the body within elastic limit $U=\sigma^{2} \mathrm{v} / 2 \mathrm{E}$ | Nm or J |
| 15 | Proof resilience | $\mathrm{U}_{\mathrm{p}}$ | $\mathrm{U}=\sigma_{\mathrm{p}}{ }^{2} \mathrm{v} / 2 \mathrm{E}$ | Nm or J |
| 16 | Modulus of resilience | - | Proof resilience per unit volume( $\left.\sigma_{p}{ }^{2} / 2 E\right)$ | Nm or J |
| 17 | Stress | $\sigma$ | Load/ Area | $\mathrm{N} / \mathrm{mm}^{2}$ |
| 18 | Types of strain | e | Tensile, Compressive , Volumetric and Shear strain | No unit |
| 19 | Types of stress | $\sigma$ | 1.Normal stress 2. Shear stress | $\mathrm{N} / \mathrm{mm}^{2}$ |
| 20 | Elasticity | - | The body tends to undergo deformation | - |
| 21 | Hooke's Law |  | Stress is directly proportional to strain within elastic limit | - |
| 22 | Factor of saftey | - | Ultimate stress/ Permissible stress | - |
| 23 | Poisson's ratio | $\mu$ | Lateral strain/Longitudinal strain | - |
| 24 | Relation between E \& C | - | $C=E / 2(1+\mu)$ | $\mathrm{N} / \mathrm{mm}^{2}$ |
| 25 | Volumetric strain | $\delta \mathrm{v}$ | ठv/v | $\mathrm{mm}^{3}$ |
| UNIT II SHEAR AND BENDING IN BEAMS |  |  |  |  |
| 26 | Shear force |  | Algebraic sum forces acting on one side of the section or other section | N |
| 27 | Beam | - | Beam is a structural member which is supported along the length and subjected to external loads acting transversely . | - |
| 28 | Bending moment for point load | M | Load X distance | N-M |
| 29 | Bending moment for udl | M | Load X Distance X Distance/2 | N-M |
| 30 | Moment of Inertia for rectangular | I | $\mathrm{I}=\mathrm{bd}^{3} / 12$ | Mm ${ }^{4}$ |
| 31 | Bending moment equation | M | $\mathrm{M} / \mathrm{I}=\sigma_{\mathrm{b}} / \mathrm{y}=\mathrm{E} / \mathrm{R}$ | N-M |


| 32 | Section modules | Z | $\mathrm{Z}=\mathrm{I} / \mathrm{y}$ | $\mathrm{mm}^{3}$ |
| :---: | :---: | :---: | :---: | :---: |
| 33 | Moment of resistance | M | $\mathrm{M}=\mathrm{obb} \mathrm{X} \mathrm{z}$ | N-mm |
| 34 | Maximum bending stress | $\sigma_{b}$ max | $\left(\mathrm{M}_{\max } / \mathrm{I}\right) \mathrm{X} \mathrm{y}$ | $\mathrm{N} / \mathrm{mm}^{2}$ |
| 35 | Section modules of rectangular | Z | $\mathrm{Z}=\mathrm{bd}^{2} / 6$ | $\mathrm{mm}^{3}$ |
| 36 | Bending Moment | M | Algebraic sum of moments | Nm |
| 37 | Cantilever beam | - | A beam is fixed at one end and other end is free | - |
| 38 | Simply supported beam | - | A beam which it has simply supported at both the ends | - |
| 39 | Overhangin g beam | - | A beam extends beyond the supports | - |
| 40 | Fixed beam | - | A Beam which is fixed at both the ends | - |
| 41 | Continuous beam | - | A beam which it has more than two supports | - |
| 42 | Types of Loading | - | Point Load, UDL , UVL | - |
| 43 | Point Load | - | A Load which is acting at an single point in a beam | - |
| 44 | UDL | - | A Load which it is distributed uniformly throughout the beam | - |
| 45 | UVL |  | A Load which varies along the length of the beam | - |
| 46 | Types of supports | - | Roller support , Pinned support, Fixed Support | - |
| 47 | Point of Contraflexu re | - | Point at which BM changes sign + ve to -ve | - |
| 48 | Sagging BM | - | Moment on left side of beam is clockwise or right side is anticlockwise | - |
| 49 | Hogging <br> BM | - | Moment on left side of beam is anticlockwise or right side is clockwise | - |
| 50 | Maximum BM | - | The shear force changes of sign or the shear force is zero | - |
| UNIT III DEFLECTION |  |  |  |  |
| 51 | Moment of inertia of circular | I | $\Pi \mathrm{d}^{4} / 64=\mathrm{I}$ | $\mathrm{mm}^{4}$ |


|  | section |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 52 | Moment of Inertia of hollow circle | I | $\Pi\left(\mathrm{D}^{4}-\mathrm{d}^{4}\right) / 64$ | mm ${ }^{4}$ |
| 53 | Section <br> Modulus of triangle | Z | $\mathrm{Z}_{\mathrm{AB}}=\mathrm{bh}^{3} / 4$ | $\mathrm{N} / \mathrm{mm}^{2}$ |
| 54 | Section modulus of 'I' section | Z | $\mathrm{Z}=\mathrm{BD}^{3}-\mathrm{bd}^{3} / 6 \mathrm{D}$ | $\mathrm{N} / \mathrm{mm}^{2}$ |
| 55 | Moment area method of slope | $\Theta$ | 1/EI X Area of BM diagram | radians |
| 56 | Moment area method of deflection | y | 1/EI X $\times$ X Area of BM diagram | mm2 |
| 57 | Deflection | y | Y=EI. y | mm |
| 58 | Slope | $\Theta$ | EI. $d y / d x=\theta$ | radians |
| 59 | Bending moment | M | EI. $\mathrm{d}^{2} \mathrm{y} / \mathrm{dx} \mathrm{x}^{2}=\mathrm{M}$ | N-M |
| 60 | Shear force | F | EI. $d^{3} y / d x^{3}=F$ | N |
| 61 | The rate of loading | W | $\mathrm{W}=E I . \mathrm{d}^{4} \mathrm{y} / \mathrm{dx}{ }^{4}$ | KN |
| 62 | Area for rectangular | A | $\mathrm{A}=\mathrm{LX} \mathrm{b}$ (Multiplication of length and breadth) | $\mathrm{m}^{2}$ |
| 63 | Area for triangular section | A | $\mathrm{A}=1 / 2 \mathrm{Xb} \mathrm{Xh}$ (Multiplications of half of the length and breadth) | $\mathrm{m}^{2}$ |
| 64 | Rectangular moment of inertia | I | $\mathrm{A}=\mathrm{bd}^{3} / 12$ | mm ${ }^{4}$ |
| 65 | Methods for <br>  <br> Deflection | - | 1. Double integration method 2. Moment area method 3. Macaulay's method | - |
| 66 | Slope for Simply supported P.L | $\Theta$ | $\Theta_{\mathrm{A}}=\Theta_{\mathrm{B}}=\mathrm{WL}^{2} / 16 \mathrm{EI}$ | radians |
| 67 | Deflection for simply | y | $\mathrm{Y}=\mathrm{WL}^{3} / 48 \mathrm{EI}$ | mm |


|  | supported <br> P.L |  |  |  |
| :---: | :--- | :--- | :--- | :---: |
| 68 | Slope for <br> UDL | $\Theta$ | Ө = WL²/24EI | radians |
| 69 | Deflection <br> for UDL | y | y =5/384*WL3/EI |  |
| 70 | Moment of <br> Inertia | I | The sum of the products of the mass of each <br> particle in the body with the square of its <br> distance from the axis of rotation | mm ${ }^{4}$ |
| 71 | Structure | - | The arrangement of and relations between <br> the parts or elements | - |
| 72 | Point load | p | The load applied to a single point |  |
| 74 | Uniformly <br> distributed <br> load | udl | A load that is distributed or spread across <br> the whole region of an element <br> varying <br> load | uvl |


| 87 | Indetermina te Structures. | - | The structures cannot be solving using conditions of equilibrium alone and additional conditions are required | - |
| :---: | :---: | :---: | :---: | :---: |
| 88 | Slopes | ( $\theta$ | Angular shift at any point of the beam between the no-load condition and loaded beam | Rad |
| 89 | Deflections | $\delta$ | The degree to which a structural element is displaced under a load | mm |
| 90 | Plane frame | - | The structures constructed with straight elements connected together by rigid and/or hinged connections | - |
| 91 | Rigid joined frame | - | The load-resisting skeleton constructed with straight or curved members interconnected by mostly rigid connections | - |
| 92 | Pin joined frame |  | Generally, transfer the applied loads by inducing axial tensile or compressive forces in the individual members | - |
| 93 | Portal frame |  | A rigid structural frame consisting essentially of two uprights connected at the top by a third member | - |
| 94 | Moment at a hinged end of a simple beam | - | Zer | - |
| 95 | Unknown moments are expressed in terms of | - | Slopes $(\theta)$ and Deflections ( $\Delta$ ) | - |
| 96 | $M-\theta$ <br> relationship for a simply supported beam | - | $M / E I=4 \theta$ | - |
| 97 | Trussed Beam | - | A beam strengthened by providing ties and struts | - |
| 98 | Plane strain | - | Normal strain and shear strain directed perpendicular to the plane of body is assumed to be zero | - |
| 99 | Plane stress | - | Plane stress exists when one of the three principal stresses is zero | - |
| 100 | Maximum shear stress | $\tau$ | $\sigma_{1}-\sigma_{2} / 2$ | $\mathrm{N} / \mathrm{mm}^{2}$ |
| UNIT V TORSION OF SHAFTS AND SPRING |  |  |  |  |


| 101 | Torsional equation | - | $T / J=\frac{\tau}{R}=\frac{C \theta}{L}$ | - |
| :---: | :---: | :---: | :---: | :---: |
| 102 | Polar modulus | $\mathrm{Z}_{\mathrm{p}}$ | It is the ratio between polar moment of inertia and radius of shaft ( $\mathrm{Zp}=\mathrm{J} / \mathrm{R}$ ) | - |
| 103 | Stiffness | K | Stiffness of the spring is load required to preclude unit deflection $K=c^{4} / 64 R^{3} n$ | $\mathrm{N} / \mathrm{mm}$ |
| 104 | Power transmitted by shaft | P | $\mathrm{P}=\frac{2 \Pi \mathrm{NT}}{60 \times 1000}$ | Nm |
| 105 | Torque transmitted by shaft | T | $\mathrm{T}=\tau \times \frac{\Pi}{16}\left(\left(D^{4}-d^{4}\right) / \mathrm{D}\right)$ | - |
| 106 | Helical spring shear stress | $\tau$ | $\mathrm{T}=\frac{16 W R}{\Pi d^{2}}$ | $\mathrm{N} / \mathrm{mm}^{2}$ |
| 107 | Helical spring Energy stored | U | $\mathrm{U}=\left(\mathrm{ob}^{2} / 8 \mathrm{E}\right) \mathrm{X}$ Volume of spring wire | Nm |
| 108 | Stiffness coefficient $\mathrm{k}_{\mathrm{ij}}$. | - | The force developed at joint ' $i$ ' due to unit displacement at joint ' $j$ ' while all other joints are fixed | - |
| 109 | Basic equations of stiffness matrix | - | Equilibrium forces, Compatibility of displacements, Force displacement relationships | - |
| 110 | Stiffness <br> matrix <br> method | - | The displacements that occur in the structure are treated as unknowns | - |
| 111 | Stiffness | k | Resistance offered by member to a unit displacement or rotation at a point | N/m |
| 112 | Stiffness <br> factor | k | Moment required to rotate the end while acting on it through a unit rotation | N/m |
| 113 | Force | F | The push or pull on an object with mass that causes it to change velocity (to accelerate) | KN |
| 114 | Shaft | - | Equal and opposite torques are applied at the two end of the shaft | - |
| 115 | Torque | T | Product of force and radius of the shaft | Nmm |
| 116 | Power | P | T * $\omega$ | KW |
| 117 | Types of springs | - | Leaf Spring, Helical Spring | - |
| 118 | Laminated Spring | - | To absorb shocks in railway wagons | - |
| 119 | Helical spring | - | Thick spring wires coiled into a helix | - |


| 120 | Types of <br> Helical <br> spring | - | Closed coiled spring, Open coiled spring | - |
| :---: | :---: | :---: | :--- | :---: |
| 121 | Deflection <br> of spring | $\delta$ | $\delta=64 \mathrm{WR}^{3} \mathrm{n} / \mathrm{Cd}^{4}$ | mm |
| 122 | Stiffness of <br> spring | s | $\mathrm{Cd}^{4} / 64 \mathrm{WR}^{3} \mathrm{n}$ | $\mathrm{N} / \mathrm{mm}$ |
| 123 | Spring <br> index | C | Ratio of mean diameter to diameter of wire | - |
| 124 | Solid length <br> 125 | Function of <br> spring | - | The length of the spring under maximum <br> compression |


| Placement Questions |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { S.N } \\ \mathbf{o} \end{gathered}$ | Term | Notation (Symbol) | Concept/Definition/M eaning/Equation/ Expression | Units |
| 126 | Sum of distribution factors at a join |  | 1 | - |
| 127 | In the displacement method of structural analysis, the basic unknowns are |  | Displacements | - |
| 128 | The number of simultaneous equations to be solved in the slope deflection method, is equal to |  | The number of joints in the structure | - |
| 129 | $M-\theta$ relationship for a simply supported beam | 118-1111 | $M / E I=4 \theta$ | - |
| 130 | The slope of the elastic curve at the free end of a cantilever beam | $\theta$ | $W L^{3} / 6 E I$ | Rad |
| 131 | Formula for Speed | S | Distance / Time | $\mathrm{m} / \mathrm{sec}$ |
| 132 | Formula for Time | t | Distance / Speed | sec |
| 133 | Formula for Distance | d | Speed x Time | m |
| 134 | Area of triangle | A | (Base $\times$ Height) / 2 | $\mathrm{m}^{2}$ |
| 135 | What is the area of a triangle with base 5 meters and height 10 meters? | A | 25 | $\mathrm{m}^{2}$ |


| 136 | Sum of the shape function is equal to | S | 1 | - |
| :---: | :---: | :---: | :---: | :---: |
| 137 | Top most part of an arch is called | - | Crown | - |
| 138 | Shape of three hinged arch is always | - | Parabolic | - |
| 139 | Degree of indeterminacy of a fixed arch | D.O.I | 3 | - |
| 140 | Degree of indeterminacy of a two hinged arch | D.O.I | 2 | - |
| 141 | Degree of indeterminacy of a three hinged parabolic arch | D.O.I | 0 | - |
| 142 | Avera ge |  | Sum of observations / Number of observations | - |
| 143 | Specific Gravity of water | G | 1 | - |
| 144 | Density of aggregate | $\rho$ | 1200-1750 | $\mathrm{kg} / \mathrm{m}^{3}$ |
| 145 | Density of Concrete (R.C.C) | $\rho$ | 2500 | $\mathrm{kg} / \mathrm{m}^{3}$ |
| 146 | Density of Concrete (P.C.C) | $\rho$ | 2400 | $\mathrm{kg} / \mathrm{m}^{3}$ |
| 147 | The density of steel is in the range of | $\rho$ | 7750 and 8050 | $\mathrm{kg} / \mathrm{m}^{3}$ |
| 148 | Flexural Rigidity | H1] | Ex I | N.m ${ }^{2}$ |
| 149 | The process of subdividing the given body into a number of elements is called | Or | Discretization | - |
| 150 | A numerical technique for solving boundary value problems is | - | Finite element method | - |

## Faculty Team Prepared

## Signatures

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